

Cours du 21 octobre 2022

Electrotechnique : alimentation et machines

Partie 2. Convertisseurs

Olivier Gras

CPGE PSI / L3 GECCLEERE



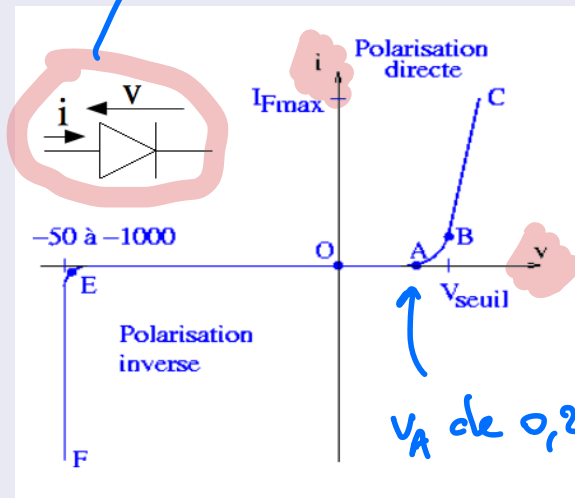
2.A Redressement de tensions sinusoïdales

2.1 diode

On va utiliser beaucoup de circuits comportant des diodes \rightarrow convention "récepteur" (v et i opposés).

Caractéristique

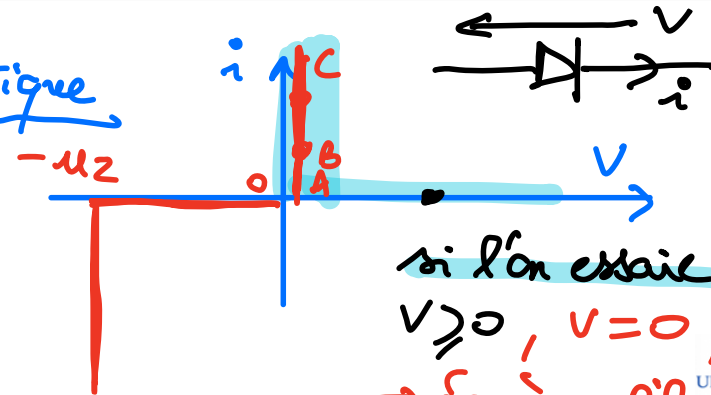
Trace de $i = f(v)$



d'où schématisation de la caractéristique

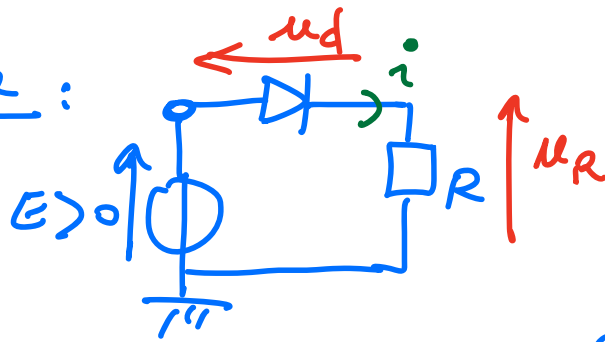
u_Z : tension ZENER

\hookrightarrow diode Zener



si l'on essaie d'imposer $v \geq 0$, $v = 0$, $i \neq 0$ (et $i > 0$)
 \Rightarrow Eq. à un fil ($R=0$)

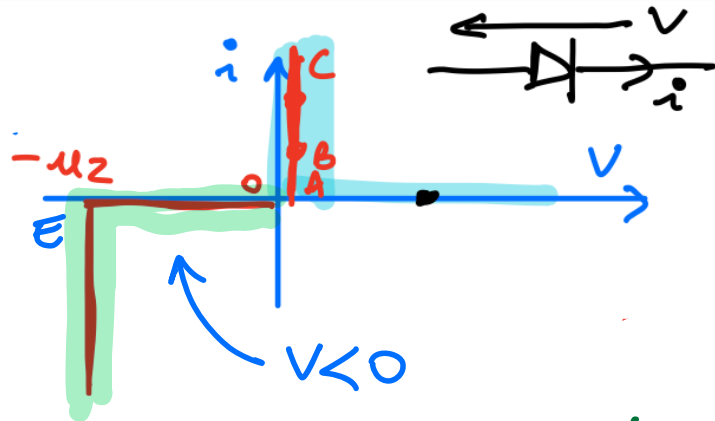
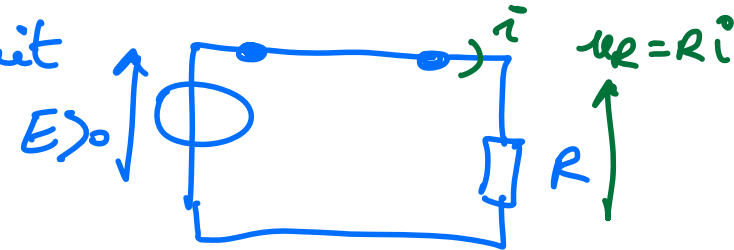
exemple :



si $u_d > 0$ (faible) \Rightarrow diode est "passante" ($i \neq 0$)

et on dit $u_d \approx 0 \Rightarrow$ fil

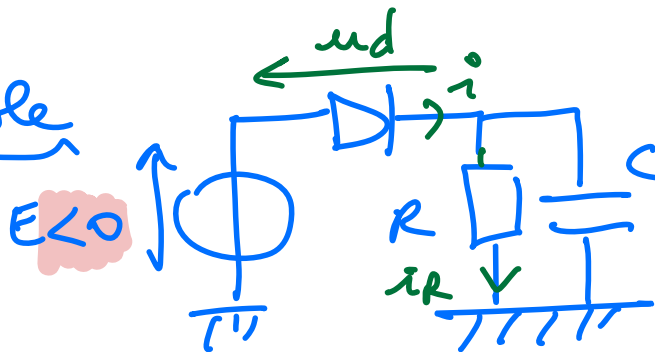
donc le circuit



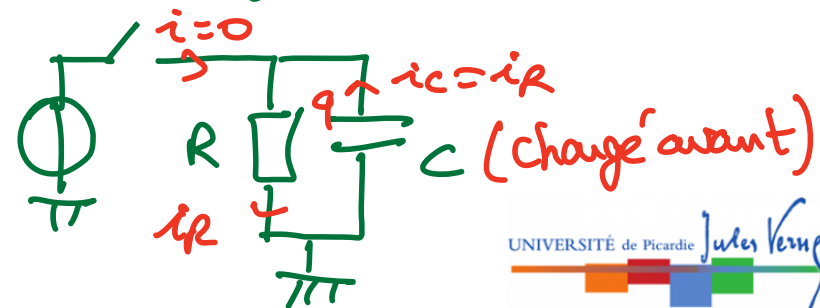
$V_E < V < 0 \Rightarrow i = 0$

la diode s'oppose au passage du courant \Rightarrow interrupteur ouvert.

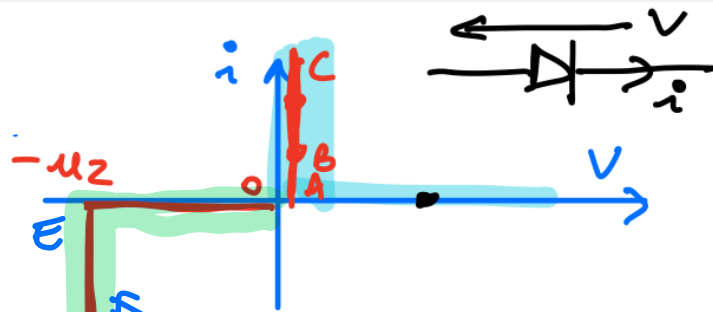
exemple



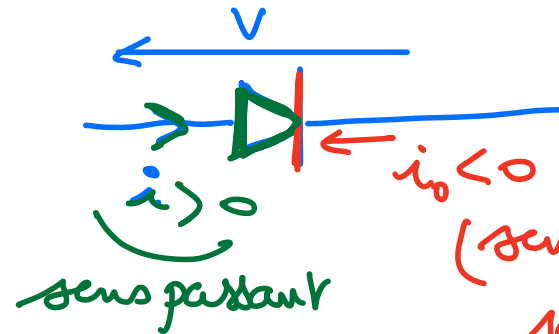
Dans le cas $V_E < u_d < 0$



Rem



$V = -u_Z$ (on "n'arrive pas" à avoir V plus basse que $-u_Z$).
 $i \neq 0$
 $i < 0$

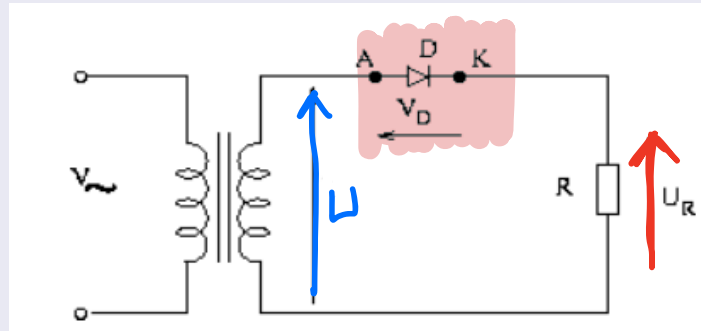


$i_0 < 0$ bloqué par |
 (sens bloqué)
 sauf "avalanche"
 du sens bloqué (Équ.
 à un éclair dans l'air).

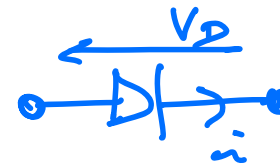
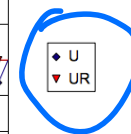
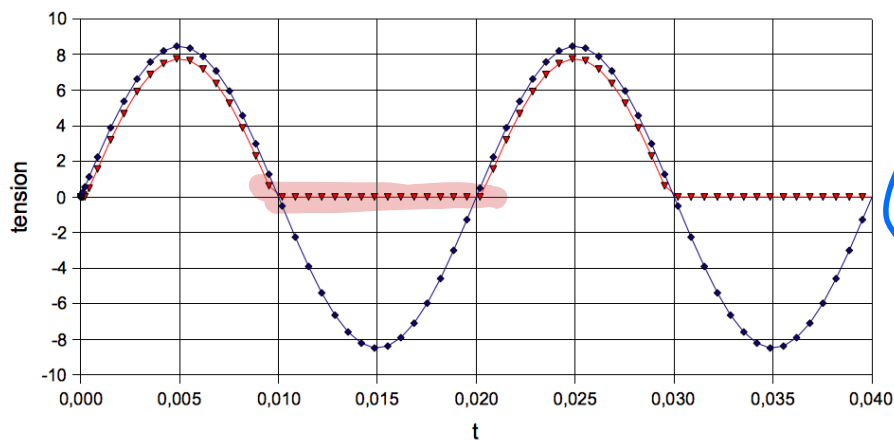
2.A Redressement de tensions sinusoïdales

2.2 redressement monoalternance

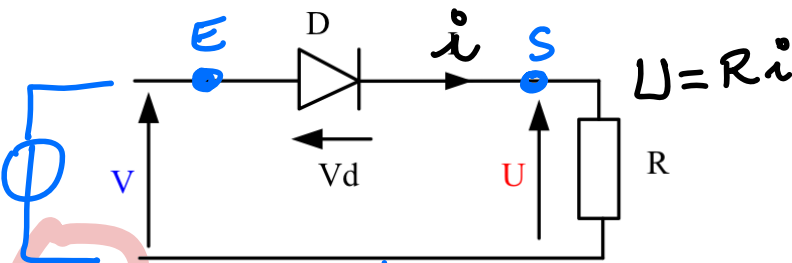
Montage



Redressement simple alternance

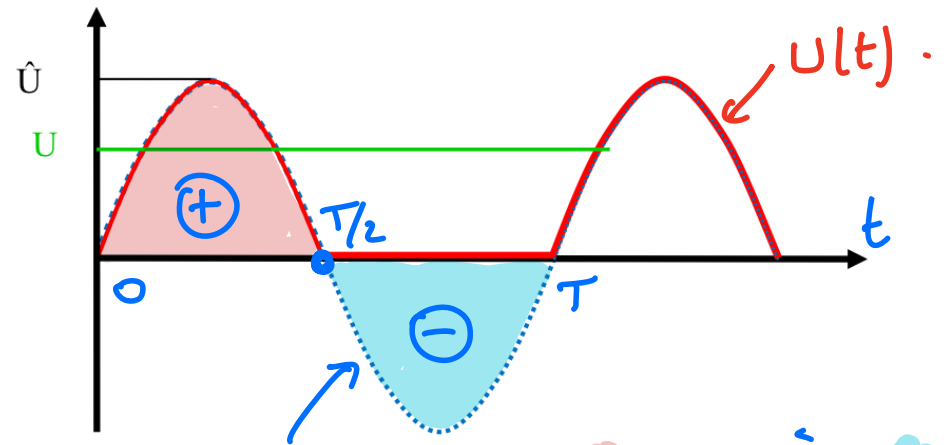


$i_D > 0$
 $i_D < 0$



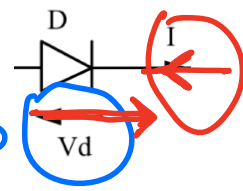
$V_d = V_E - V_S$
 $= V - U$
 avec $U = V_S - 0$
 $V = V_E - 0$

souvent la masse
 neutre
 pas un vrai
 zéro.
 Terre
 zéro volt



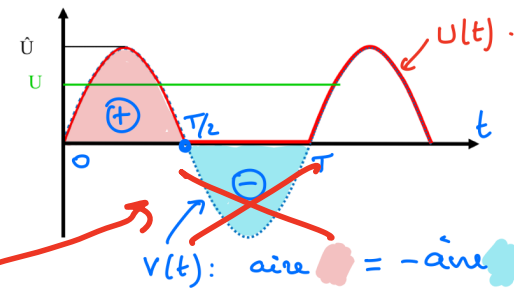
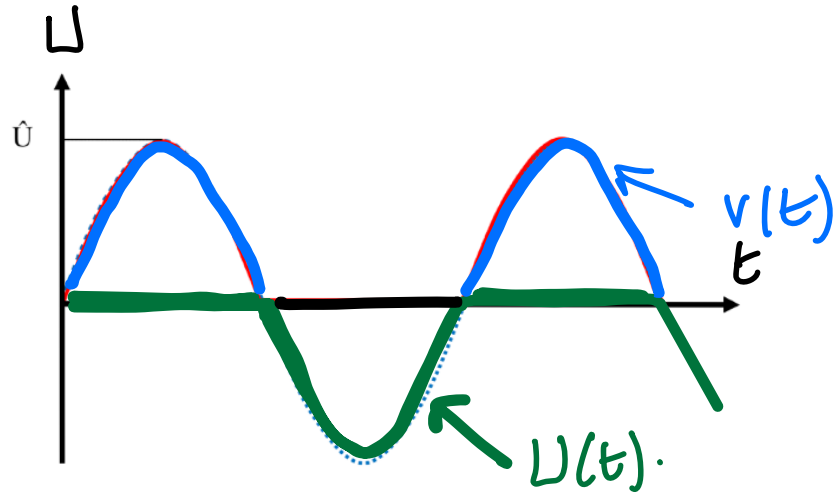
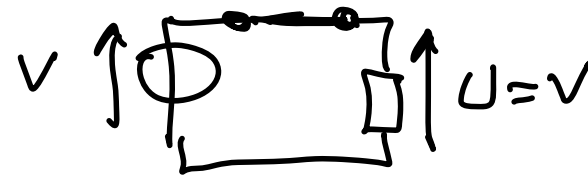
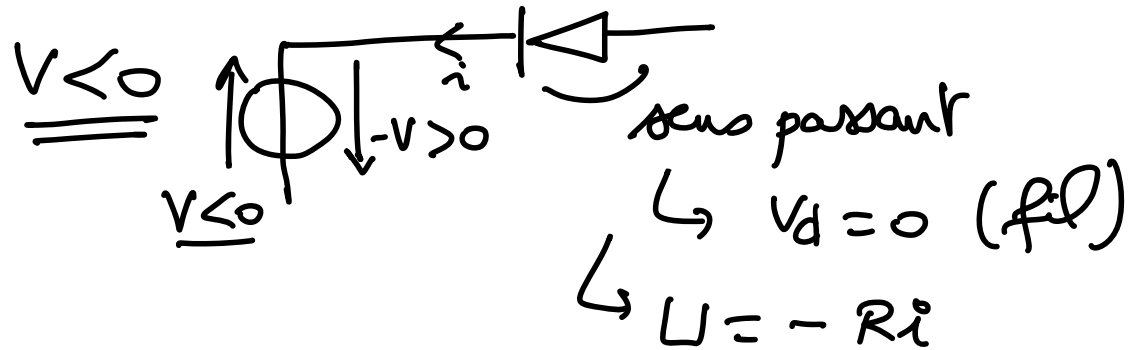
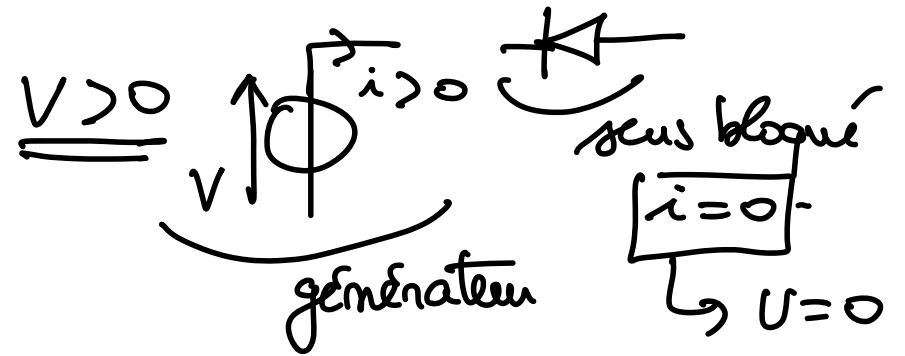
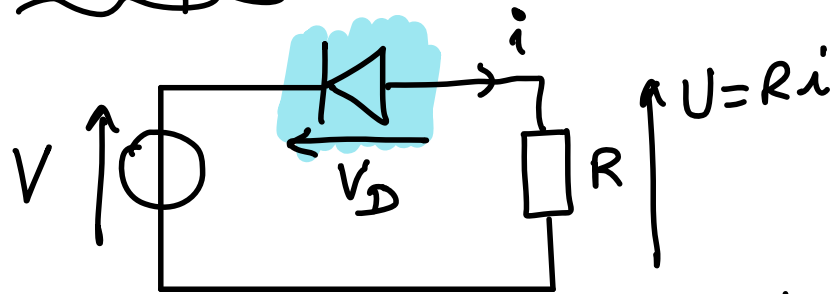
$V(t)$: aire $\text{red} = -\text{aire} \text{blue}$
 \hookrightarrow somme nulle
 $\Rightarrow \bar{V} = 0$ (moyenne)
 (car $\bar{V} = \frac{1}{T} \int_0^T V(t) dt$)

$t = \frac{T}{2} \Rightarrow V = 0$
 de $0 \text{ à } \frac{T}{2} \Rightarrow U = V$ (diode passante)
 à partir de $\frac{T}{2}$, $V(t) < 0$
 $\hookrightarrow V_d = +V - 0 < 0$



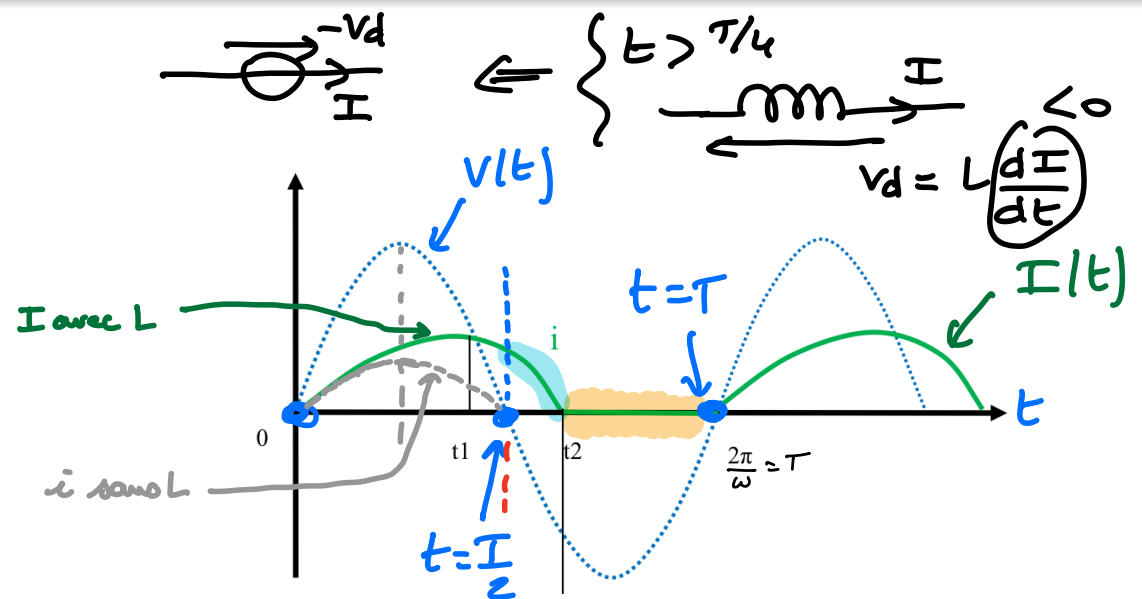
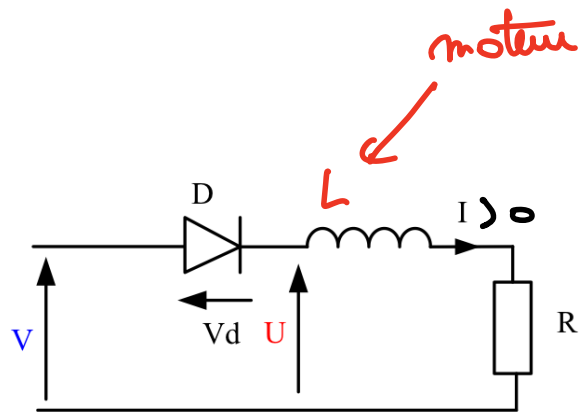
$V_d = V - U = 0$
 sens bloqué $\Rightarrow i = 0 \Rightarrow U = 0$

Exemple

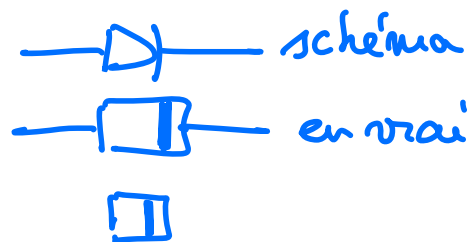
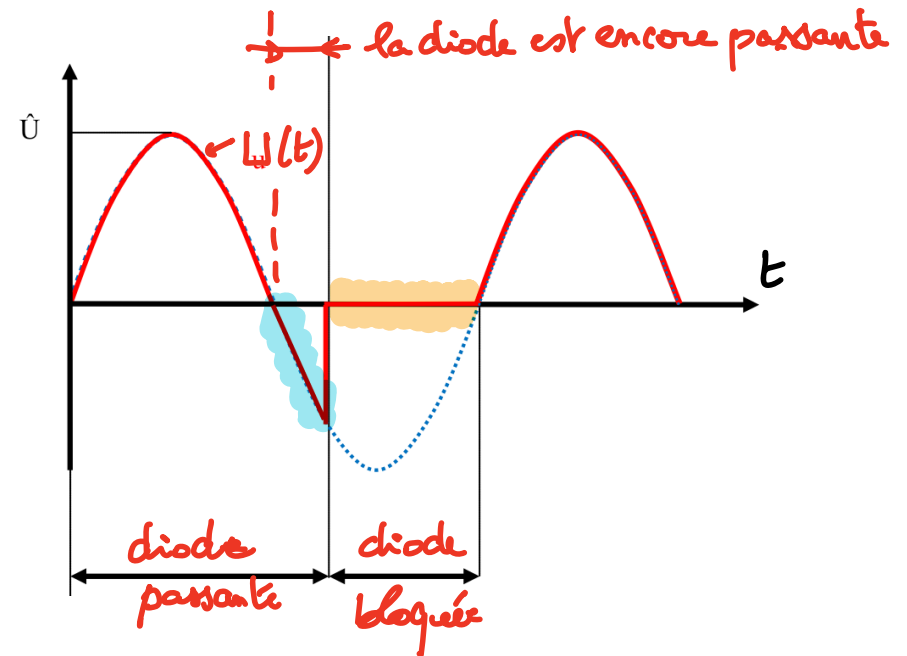
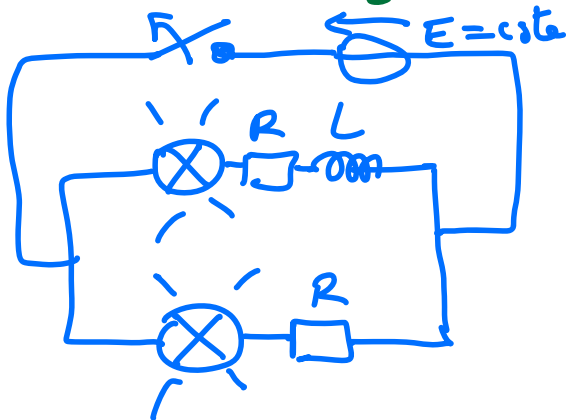


! "redressement" monoalternance.

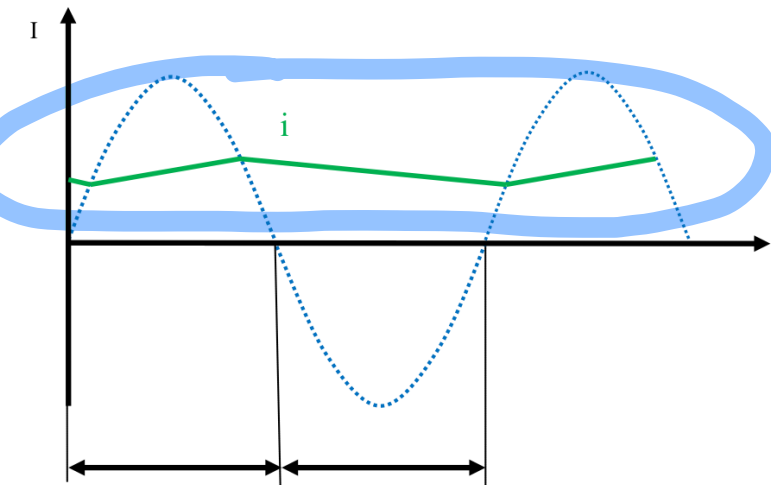
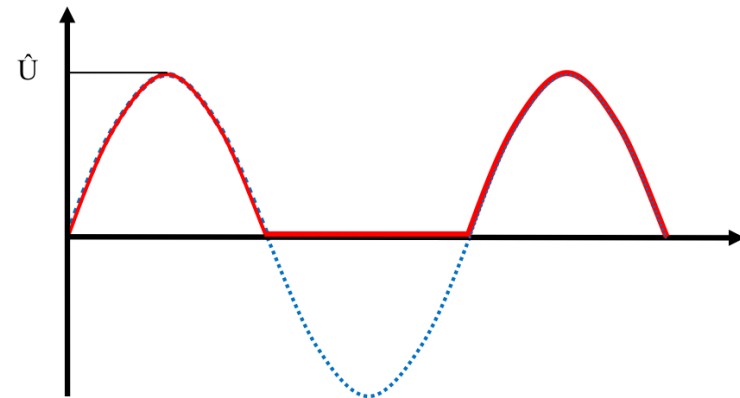
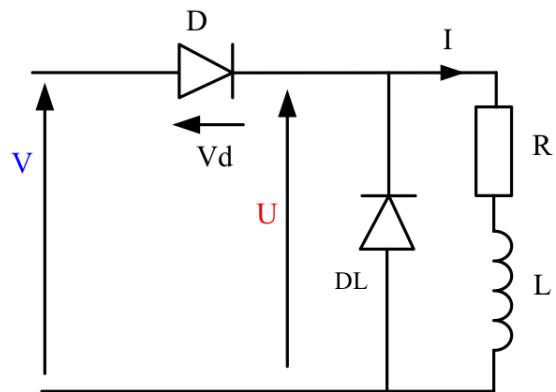
on perd une alternance



Énergie stockée $\mathcal{E} = \frac{1}{2} L I^2$
 donc $0 < t < \frac{T}{2}$, $I \uparrow \Rightarrow \mathcal{E} \uparrow$



4 HACHEURS



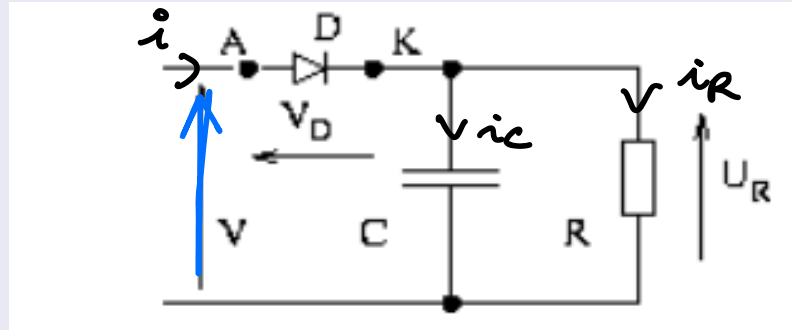
$I \approx \text{cste}$
pour alimenter
un rotor (L)

2.A Redressement de tensions sinusoïdales

2.3 redressement monoalternance : filtrage

Montage

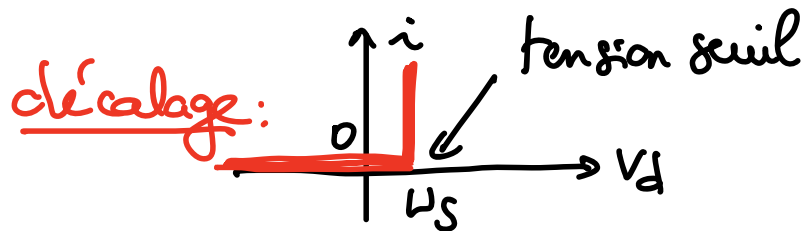
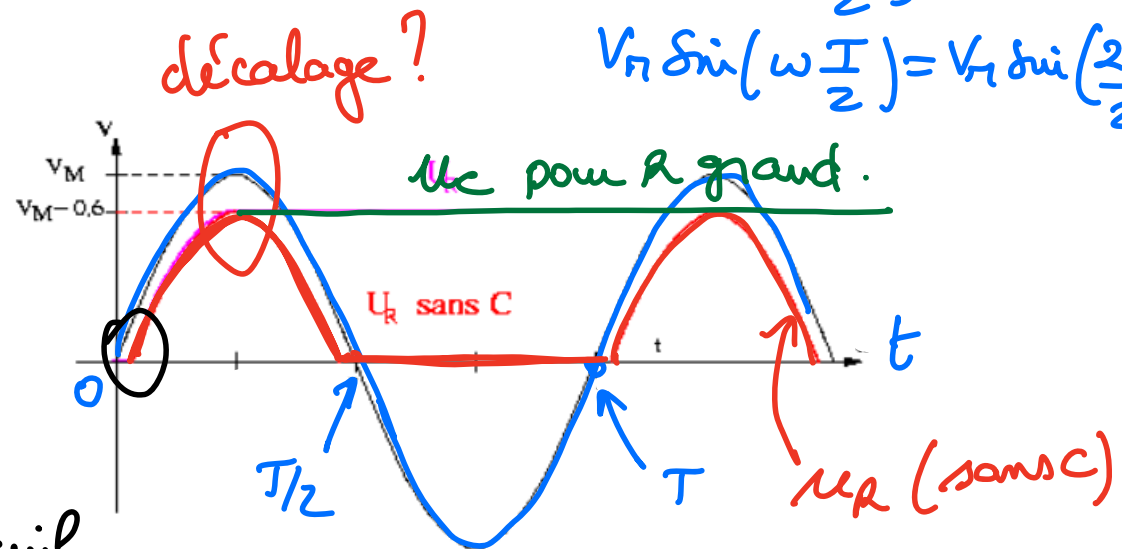
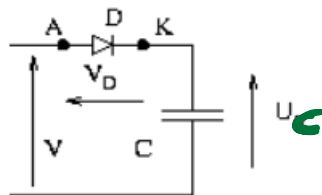
$$\begin{cases} \omega = 2\pi/T \\ v(t) = V_M \sin(\omega t) \end{cases}$$



Deux cas à analyser : 1) diode passante 2) diode bloquée $V(t = \frac{T}{2}) = 0$?

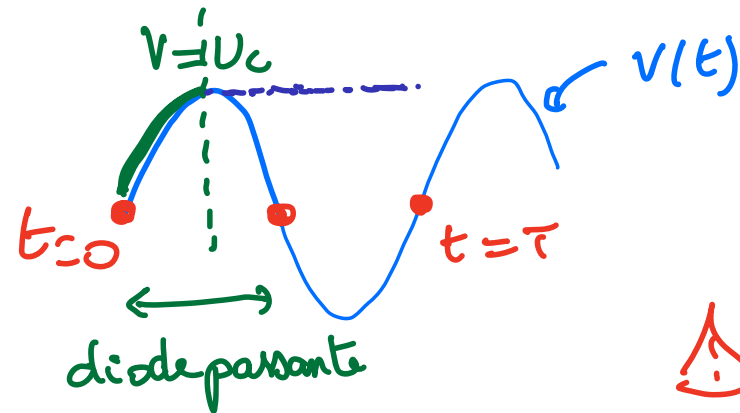
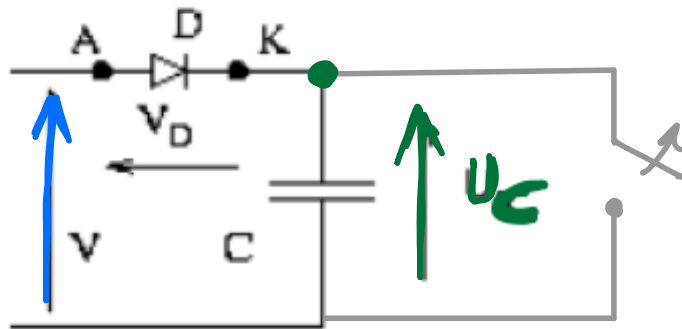
Cas idéal : $R \rightarrow \infty$

Si R est grand

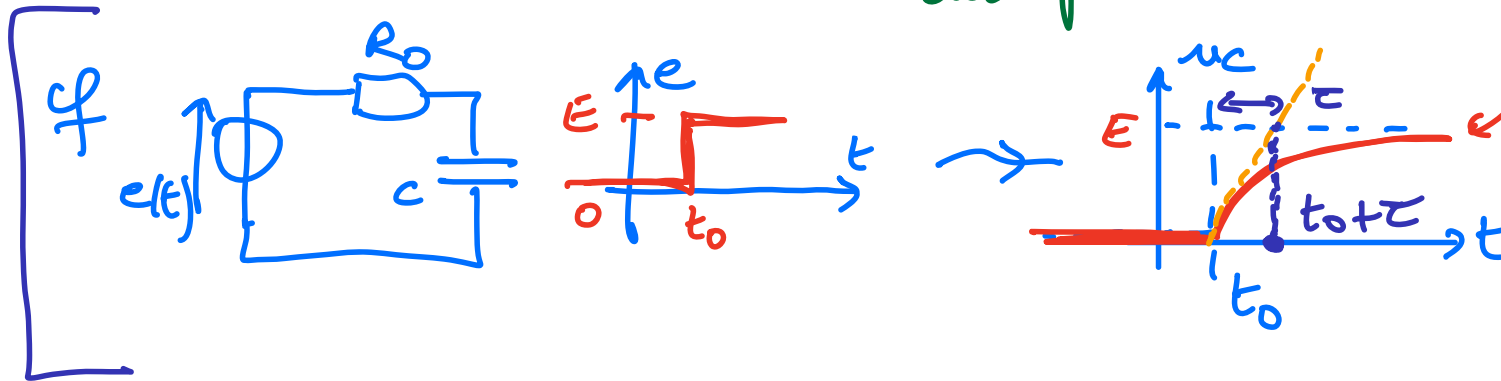


Si R est grand

$U_R = R i_R \Rightarrow i_R = \frac{U_R}{R} \xrightarrow{R \rightarrow \infty} 0$ donc interruption ouverte



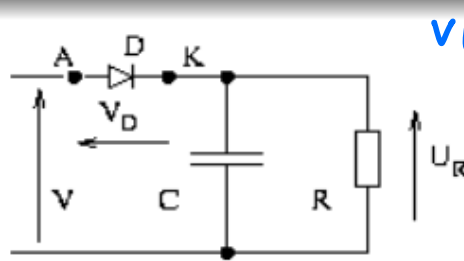
$\lim_{t \rightarrow \infty} e^{-t/\tau} = 0$
 $u_C = E(1 - e^{-t/\tau})$
 avec $\tau = R_0 C$.



donc ici $R_0 = 0$ donc $\tau = 0$ donc la "charge" de C est instantanée.

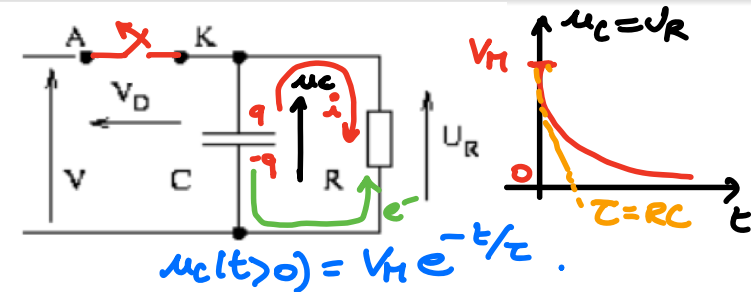
2.A Redressement de tensions sinusoïdales

2.3 redressement monoalternance : filtrage



$$v(t) = V_M \sin(\omega t)$$

$$\left. \begin{array}{l} R \neq 0 \\ R \neq \infty \end{array} \right\}$$

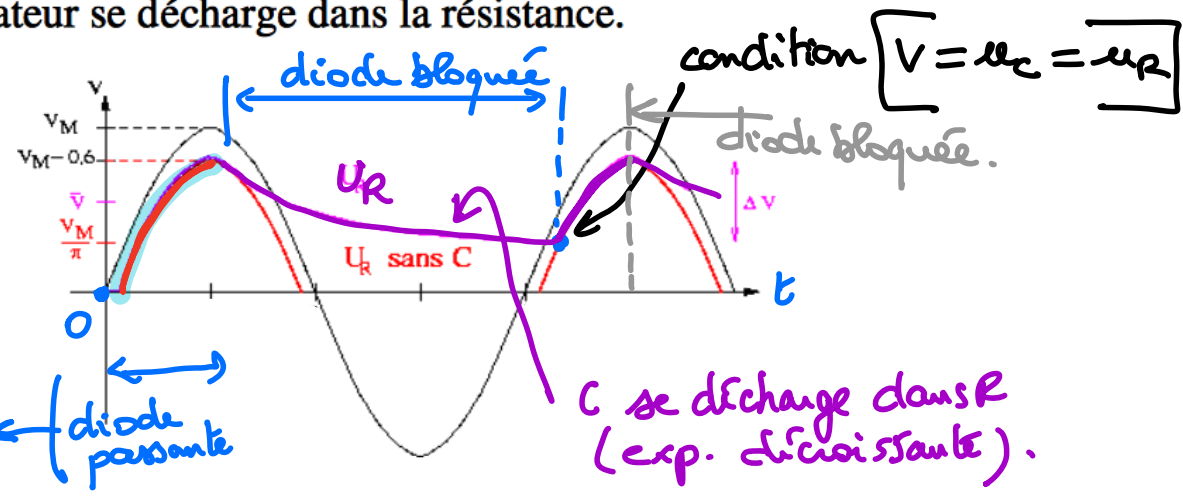


Cas d'une résistance non nulle

Quand la diode est bloquée le condensateur se décharge dans la résistance

Dès que la diode se bloque, le condensateur se décharge dans la résistance.

$$\Delta V < V_{M'}, \quad \bar{V} > 2 \frac{V_M}{\pi}$$



$$\boxed{V = u_C = U_R} \leftarrow \left. \begin{array}{l} v_d = 0 \\ i \neq 0 \end{array} \right\} \leftarrow \text{diode passant}$$

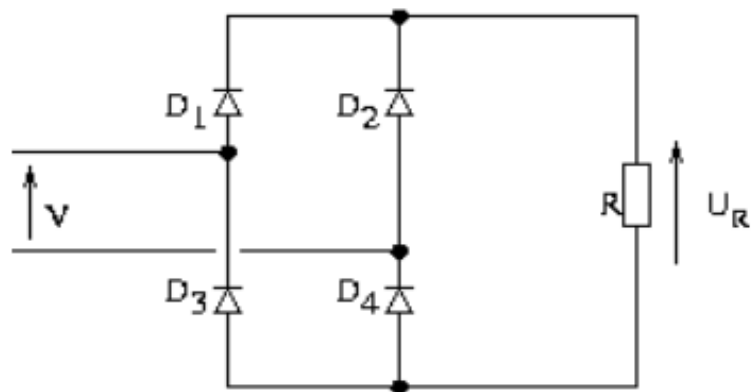
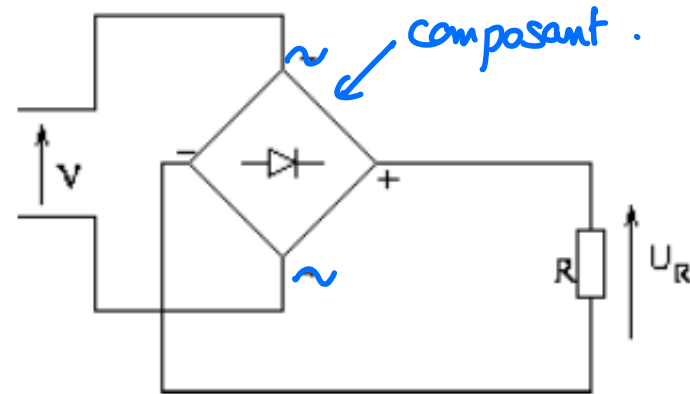
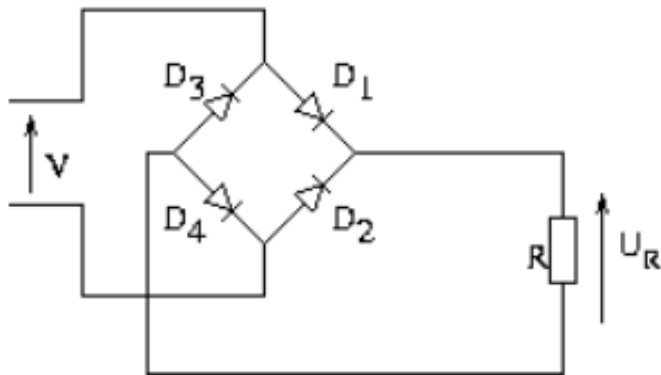
2.A Redressement de tensions sinusoïdales

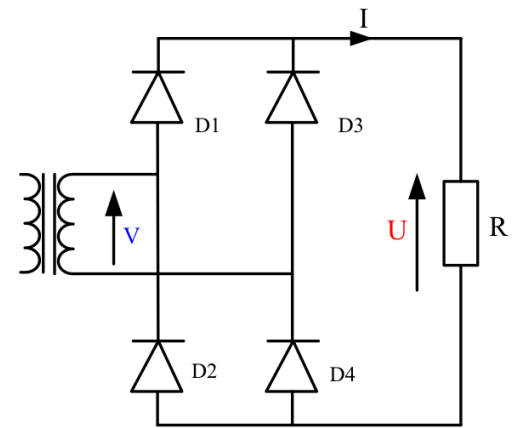
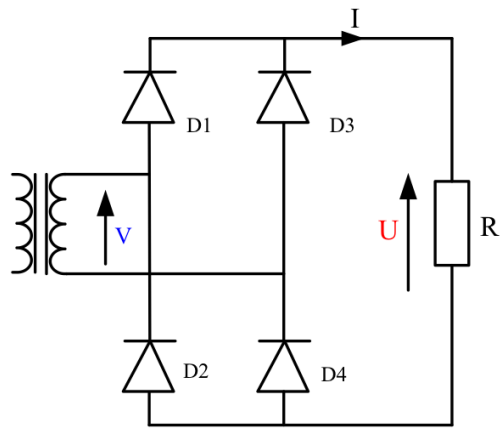
2.4 redressement bialternance : montage

Montage : utilisation de l'inversion du courant

On maintient un courant de même signe dans la résistance.

Pont de GRAETZ





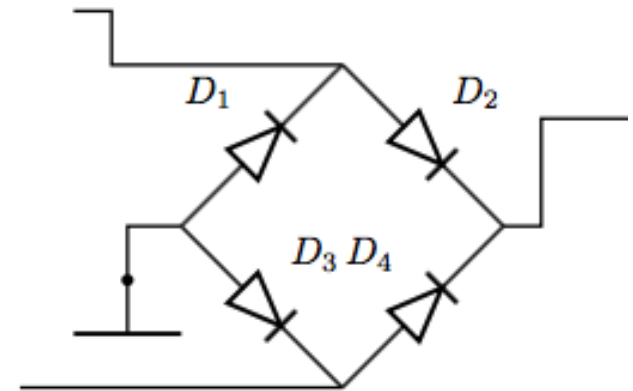
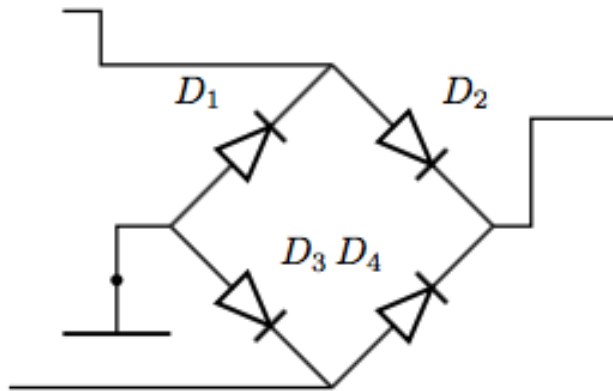
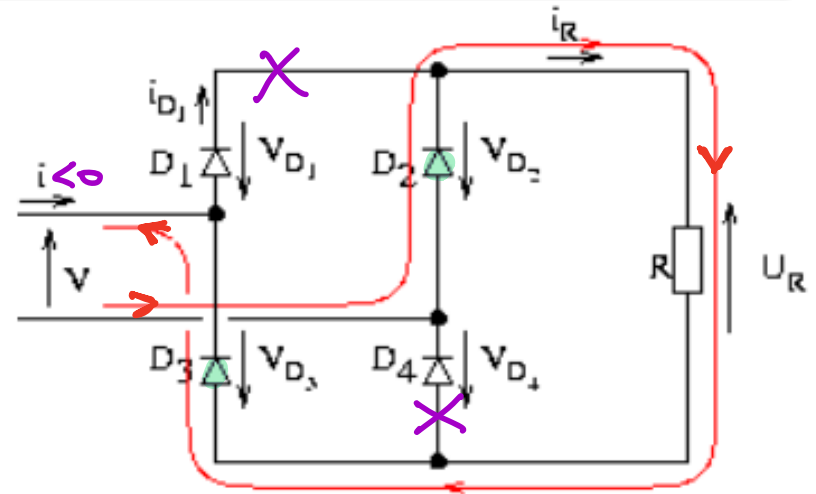
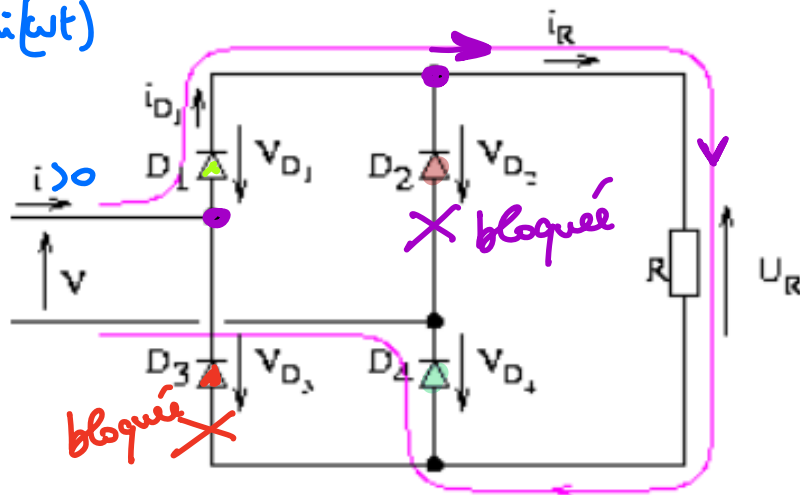
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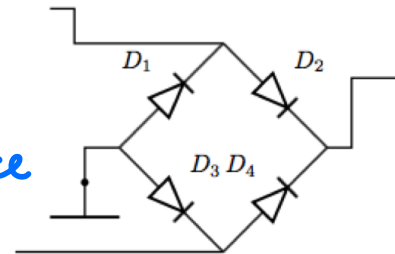
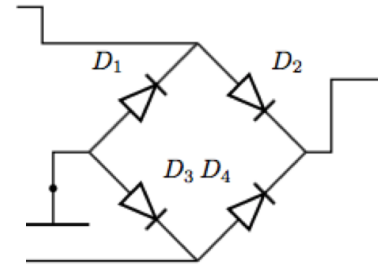
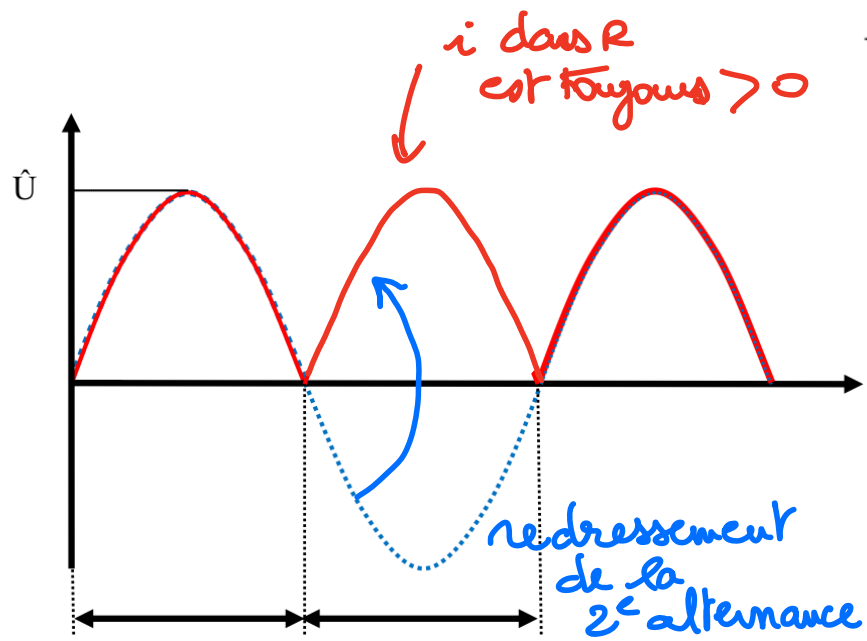
2.4 redressement bialternance : fonctionnement

Parcours du courant

On maintient un courant de même signe dans la résistance.

$$v(t) = V_m \sin(\omega t)$$





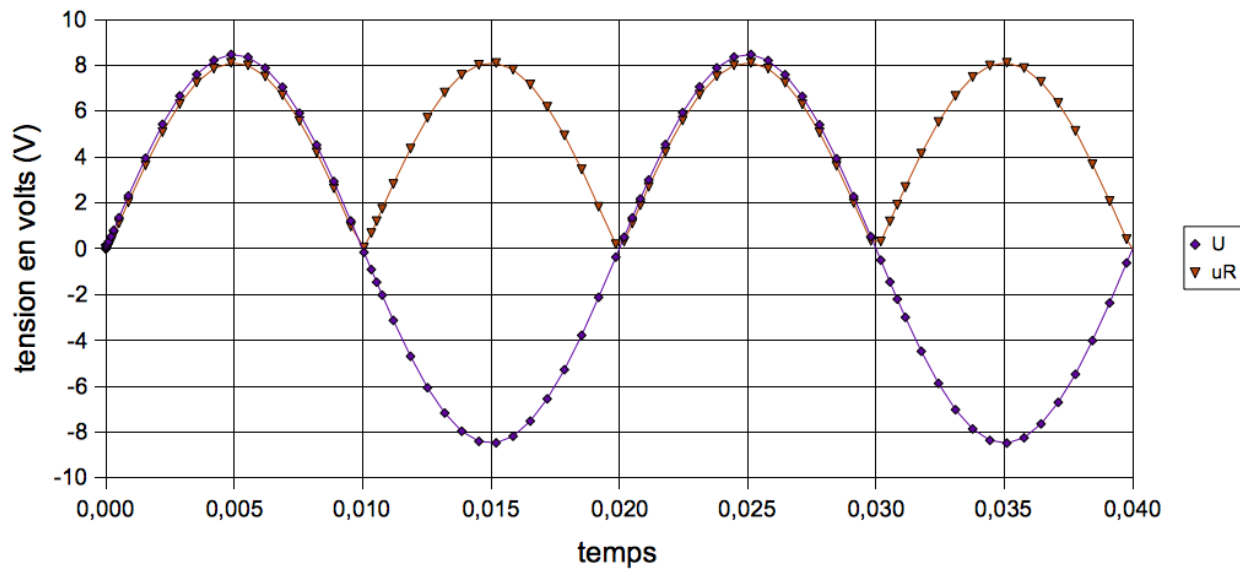
2.A Redressement de tensions sinusoïdales

2.5 redressement bialternance : signaux

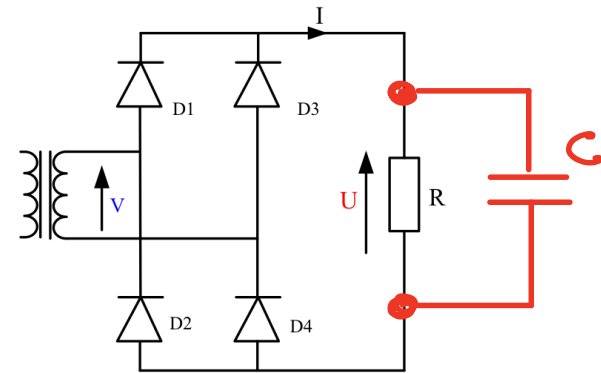
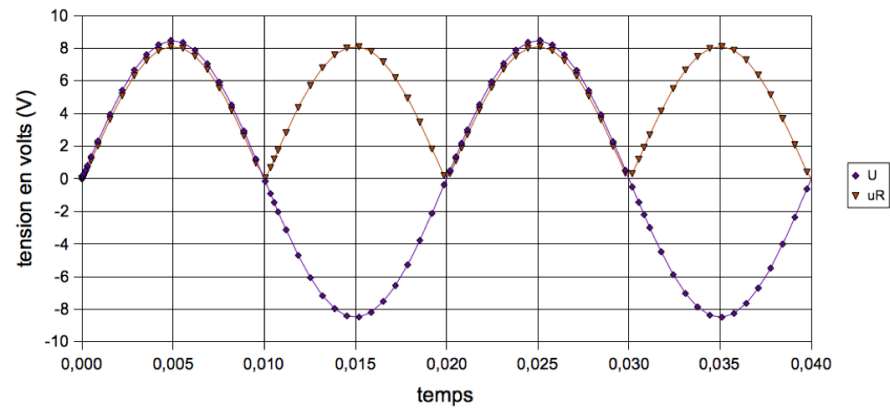
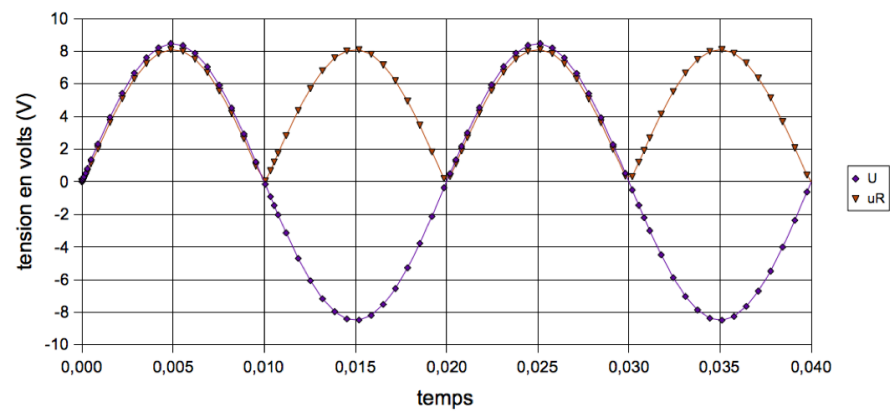
forme du signal bialternance

Pour un signal d'entrée $v_e(t) = V_m \sin(\omega t)$, on obtient la valeur absolue si les tensions seuils des diodes sont négligeables

Redressement double alternance



Intérêt : la valeur moyenne est non nulle.
But ultérieur : lissage de cette tension.

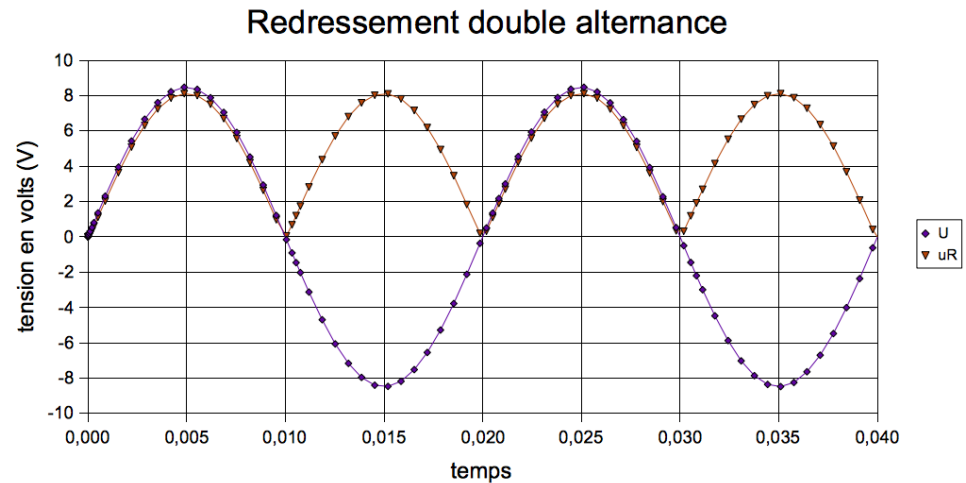
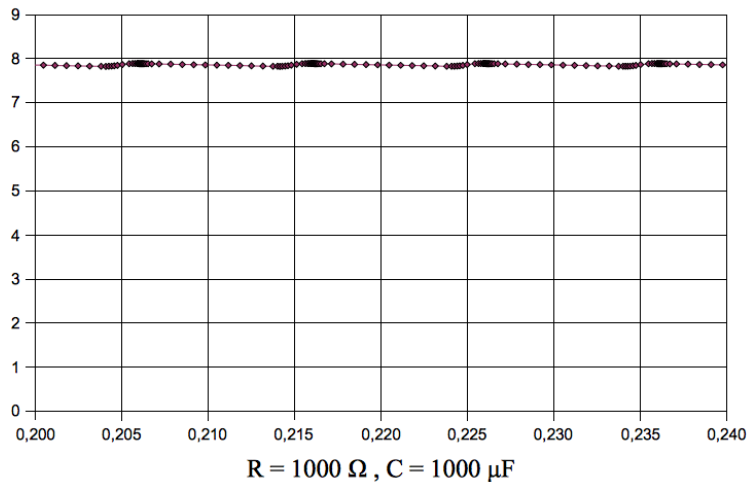
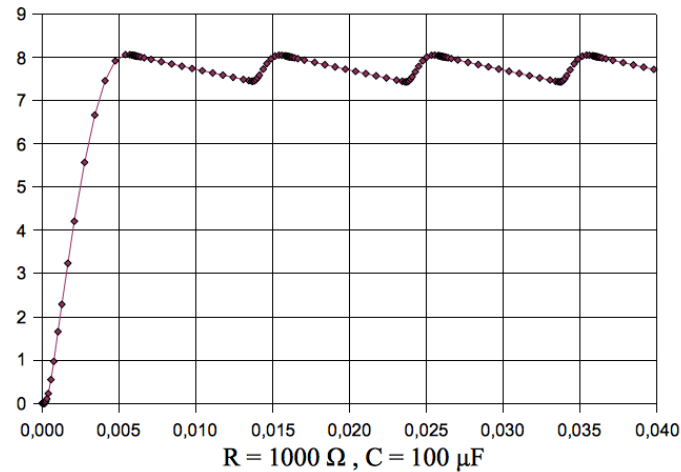
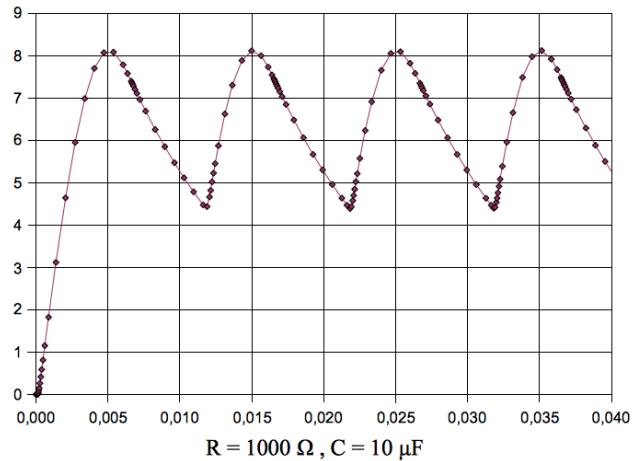


2.A Redressement de tensions sinusoïdales

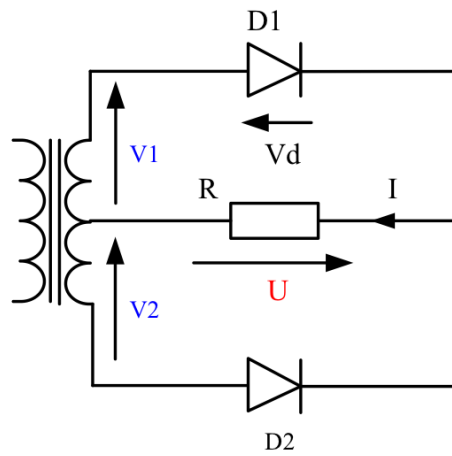
2.6 redressement bialternance : lissage

forme du signal bialternance

On utilise un condensateur en parallèle avec la charge R



Autre redressement :



redressement triphasé simple alternance (P3)

